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COMPUTER PROGRAM FOR EVALUATION  
OF BLOCH-GRUENEISEN PARAMETERS  
OF METALS AND EVALUATION OF  
ELECTRICAL RESISTIVITY OF TANTALUM  
AS A FUNCTION OF TEMPERATURE

*by Thor T. Semler and John P. Riehl*

*Lewis Research Center  
Cleveland, Ohio 44135*

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16. Abstract  A computer program has been written for the least squares evaluation of the parameters in the Bloch-Grueneisen relation for "ideal" electrical resistivity of metals. The program input is experimental measurements of resistivity and temperature. The constants associated with tantalum have been determined by using this code and several experimental measurements of the electrical resistivity of tantalum.					
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COMPUTER PROGRAM FOR EVALUATION OF BLOCH-GRUENEISEN PARAMETERS  
OF METALS AND EVALUATION OF ELECTRICAL RESISTIVITY  
OF TANTALUM AS A FUNCTION OF TEMPERATURE

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Lewis Research Center

SUMMARY

A computer program using nonlinear functional minimization has been written to obtain least squares solutions, from experimental measurements, for the constant terms of the Bloch-Grueneisen relation

$$\rho_T(T) = A \left( \frac{T}{\theta_R} \right)^5 \int_0^{\theta_R/T} \frac{x^5 dx}{(e^x - 1)(1 - e^{-x})}$$

where  $\rho_T(T)$  is the "ideal" electrical resistivity of metals as a function of temperature,  $A$  is a constant of the metal,  $T$  is the temperature in K, and  $\theta_R$  is the characteristic temperature of resistivity.

The metal tantalum has been analyzed by using the code, and a typical result is  $\theta_R = 217.54$  K and  $A = 39.95$  microhm-centimeters between 10 and 250 K.

INTRODUCTION

A fundamental constant in Ohm's law is the electric resistance of the conductor  $R$ . For a particular conductor of length  $l$  (in cm) and uniform cross-sectional area  $a$  (in  $\text{cm}^2$ ),  $R$  (in ohms) may be computed as

$$R = \frac{\rho l}{a} \quad (1)$$

where  $\rho$  is the electrical resistivity in ohm-centimeters. As the electrical resistance is a quantity of great interest in both engineering and solid-state physics (refs. 1 to 3), it is important to be able to determine the electrical resistivity and then compute the resistance of a conductor.

The resistivity of a metal is a function of temperature. On approaching very low temperatures, near absolute zero, the electrical resistivity assumes a constant value (neglecting the region in which some metals become superconductors)  $\rho_0$ , called the residual resistivity. This quantity  $\rho_0$  arises from imperfections, impurities, and strains in the metal lattice and must be determined for each individual sample.

The total resistivity  $\rho$  may be divided into two portions, the residual resistivity and the temperature-dependent resistivity  $\rho_T(T)$ :

$$\rho = \rho_0 + \rho_T(T) \quad (2)$$

This division is known as Matthiessen's rule (refs. 3 and 4).

It is possible to derive a formula for the temperature-dependent resistivity  $\rho_T(T)$  over a large temperature range from certain approximations about the interactions of conduction electrons and the metallic lattice vibrations (refs. 5 to 8). The formula (3) so derived is referred to as the Bloch-Grueneisen relation

$$\rho_T(T) = A \left( \frac{T}{\theta_R} \right)^5 \int_0^{\theta_R/T} \frac{x^5 dx}{(e^x - 1)(1 - e^{-x})} \quad (3)$$

where  $A$  is a constant of the metal and  $\theta_R$  is the characteristic temperature of resistivity. The Bloch-Grueneisen relation is widely applied because it provides a good approximation for the temperature-dependent resistivity for many metals.

Because of the difficulties in the form of the relation, many rule-of-thumb techniques have been evolved by experimenters to evaluate  $A$  and  $\theta_R$  from experimental data. Unfortunately, many of these rule-of-thumb techniques are rather crude (ref. 4).

The computer program described in the section ANALYSIS allows one to compute in the least-squares sense the best values of  $A$  and  $\theta_R$  from all the experimental data one might wish to use. This computer program is then used to obtain values of  $A$  and  $\theta_R$  for metallic tantalum.

## ANALYSIS

Given values of  $\rho_T$  that have been measured as a function of temperature, one would like the values of  $\theta_R$  and  $A$  which are "best" in the least-squares sense. This means that one must form the function  $f(A, \theta) = \sum_i \left[ \rho_{T,i,\text{measured}} - \rho_{T,i,\text{calculated}} \right]^2$  and minimize it by the variation of  $\theta_R$  and  $A$ .

By the rules of ordinary calculus,  $f(A, \theta)$  without constraint obtains a local minimum or reaches a saddle point when the gradient  $\nabla f(A, \theta) = 0$  at particular values of  $A$  and  $\theta$ . For those functions  $l(x, p)$  that are linear in  $p$  the gradient requirement produces a set of simultaneous linear equations. But for functions that are nonlinear in  $p$ , this requirement is not easily met. One is confronted with a set of nonlinear simultaneous equations in  $p$  to be solved. Such is the case for the Bloch-Grüneisen equation. Its gradient has components

$$\begin{aligned} \frac{\partial f}{\partial A} = -2 \sum_{i=1}^{\text{NDP}} & \left\{ \left[ \rho_{T(T_i)} - A \left( \frac{T_i}{\theta_R} \right)^5 \int_0^{\theta_R/T_i} \frac{x^5 dx}{(e^x - 1)(1 - e^{-x})} \right] \right. \\ & \left. \left( \frac{T_i}{\theta_R} \right)^5 \int_0^{\theta_R/T_i} \frac{x^5 dx}{(e^x - 1)(1 - e^{-x})} \right\} \\ \frac{\partial f}{\partial \theta} = -2 \sum_{i=1}^{\text{NDP}} & \left\{ \left[ \rho_{T(T_i)} - A \left( \frac{T_i}{\theta_R} \right)^5 \int_0^{\theta_R/T_i} \frac{x^5 dx}{(e^x - 1)(1 - e^{-x})} \right] \right. \\ & \left. \left( -5A \frac{T_i^5}{\theta_R^6} \int_0^{\theta_R/T_i} \frac{x^5 dx}{(e^x - 1)(1 - e^{-x})} + \frac{A}{T_i} \frac{1}{\left( e^{\theta_R/T_i} - 1 \right) \left( 1 - e^{-\theta_R/T_i} \right)} \right) \right\} \end{aligned}$$

where NDP is the number of data points.

The second component was arrived at by using the chain rule and Leibnitz's rule, which is, if  $F(x) = \int_{\varphi(x)}^{\psi(x)} f(x,y)dy$  is continuously differentiable, then

$$F'(x) = \int_{\varphi(x)}^{\psi(x)} \frac{\partial}{\partial x} f(x,y)dy - f(x, \varphi(x)) \cdot \varphi'(x) + f(x, \psi(x)) \cdot \varphi'(x)$$

To accomplish the unconstrained function minimization, the method of Fletcher and Powell was employed (ref. 9). The Fletcher and Powell algorithm is a modification of a method of Davidon (ref. 10). It is a powerful and general method for finding the local minimum of a general function  $f(x)$ .

Central to the method is a symmetric positive definite matrix  $\mathcal{H}_i$  which is updated at each iteration  $i$ . The current direction of motion  $\vec{S}_i$  is supplied by  $\mathcal{H}_i$  when it is multiplied with the current change gradient vector. An iteration is described by the following: If  $\mathcal{H}_0$  is any positive definite matrix, usually the identity matrix  $\mathcal{I}$ , on the first iteration only, then

$$\vec{S}_i = -\mathcal{H}_i \nabla f(\vec{x})|_{\vec{x}=\vec{x}_i}$$

Choose  $\alpha = \alpha_i$  by minimizing  $f(\vec{x}_i + \alpha \vec{S}_i)$ ; this straight line minimization is done with cubic interpolation:

$$\vec{\sigma}_i = \alpha \vec{S}_i$$

$$\vec{x}_{i+1} = \vec{x}_i + \vec{\sigma}_i$$

$$\mathcal{H}_{i+1} = \mathcal{H}_i + \mathcal{A}_i + \mathcal{B}_i$$

where the matrices  $\mathcal{A}_i$  and  $\mathcal{B}_i$  are defined by

$$\mathcal{A}_i = \frac{\vec{\sigma}_i(\vec{\sigma}_i)}{(\vec{\sigma}_i)\vec{y}_i}, \quad \vec{y}_i = \nabla f(\vec{x}_{i+1}) - \nabla f(\vec{x}_i)$$

and

$$\mathcal{B}_i = \frac{-\mathcal{H}_i \vec{y}_i \vec{y}_i \mathcal{H}_i}{\vec{y}_i \mathcal{H}_i \vec{y}_i}$$

$\vec{y}_i$  being the transpose of  $\vec{y}_i$ .

The numerators of  $\mathcal{A}_i$  and  $\mathcal{B}_i$  are both matrices, while the denominators are scalars. Fletcher and Powell (ref. 9) prove the following:

(1) The matrix  $\mathcal{H}_i$  is positive and definite for all  $i$ . As a consequence, the method will always converge since

$$\frac{d}{d\alpha} f(\vec{x}_i + \alpha \vec{S}_i) \big|_{\alpha=0} = -\vec{\nabla} f(\vec{x}_i) \cdot \vec{S}_i < 0$$

That is, the function  $f$  is initially decreasing along the direction  $\vec{S}_i$ . So that the function can be decreased at each iteration by minimizing along  $\vec{S}_i$ .

(2) When the method is applied to the quadratic matrix equation  $q(\vec{x}) = a + \vec{b}\vec{x} + \vec{x}\mathcal{A}\vec{x}$  and  $\vec{x}$  is a vector of  $n$  dimensions,

(a) The directions  $\vec{S}_i$  (or equivalently  $\vec{\sigma}_i$ ) are  $\mathcal{A}$  conjugate, that is,  $\vec{S}_i \cdot \vec{S}_j = 0$  for  $i \neq j$ . This condition leads to a minimum in  $n$  steps.

(b) The matrix  $\mathcal{H}_i$  converges to the inverse of the Hessian, that is, the matrix of second partial derivatives after  $n$  iterations,  $\mathcal{H}_n = \mathcal{A}^{-1}$ . When applied to a general function  $f(\vec{x})$ ,  $\mathcal{H}_i$  tends to the inverse of the Hessian evaluated at the minimum. The Fletcher-Powell algorithm is represented by the flow chart in figure 1.

## CALCULATION OF BLOCH-GRUENEISEN RELATION

The integral portion of the Bloch-Grueneisen relation was calculated by using a modified Simpson's rule integration scheme. This scheme, programmed as subprogram SIMPS1, adapts to regions where more points are required to obtain an accurate result. Had the integral been too expensive (in terms of computer time) to compute, a spline approximation to tabular results of the integral could have been made. It was our experience that the Bloch-Grueneisen relation and the ensuing least-squares function could be calculated in very little time by using the modified Simpson's rule routine.

In the program the exponent 5 of equation (3) may be varied, as indicated in the comments card. This permits the user to use other than a fifth-order Bloch-Grueneisen relation. Input is described in appendix A. A flow chart of the main program is shown in figure 2. A listing of the program is given in appendix B.

## DATA USED IN EVALUATION OF TANTALUM

Experimental measurements of the electrical resistivity of the metal tantalum have been analyzed by using this code. Only experimental values of the electrical resistivity

in the temperature region from above 0 K (actually 10 K as tantalum is a superconductor) to about 400 K have been used in the program. The values have been taken from this region since the least-squares fit of the parameters is relatively insensitive to data outside the range 0 K to a few times  $\theta_R$  K.

### Cox Data in Temperature Range 77 to 373 K

Cox in 1943 performed a series of experiments to determine both the thermal and electrical conductivities of tungsten and tantalum (ref. 11). This series of experiments yielded three values of the electrical resistivity of tantalum.

The sample used was a tantalum wire about 40 centimeters long and about 0.0254 centimeter in diameter. The wire was aged by passing as high a current as possible through it without evaporating it. The tantalum sample was aged at both 1800° and 2000° C for a total time of 2750 hours. The resistance at zero power input was plotted at a function of aging time. The resistance decreased rapidly at first and finally reached a constant value; at that point, aging was ceased. The chemical purity quoted for the sample was 99.9 percent.

After aging, the sample was immersed in baths of boiling liquid nitrogen, ice water, and boiling water, readings of voltage and current across the sample were taken, and the resistivity was computed; these data are given in table I.

### White and Woods Data in Temperature Range 10 to 295 K

White and Woods, in a series of experiments to determine the electrical and thermal resistivity of the transition elements, report 21 values of the ideal resistivity of tantalum (ref. 12). These results were obtained by subtracting the residual resistivity from the total resistivity of the sample at a temperature, and they are shown in table II.

The specimen was mounted in a cryostat. One end of the specimen was soldered to a copper post, and a specimen heater was attached to the other end. Copper wires were attached to intermediate points of the rod to act as electrical potential leads for the resistivity measurements. The specimen was surrounded by low-pressure helium gas to preserve temperature equilibrium in the cryostat.

The purities of the three samples of tantalum used are quoted as 99.9 percent, "high", and 99.9 percent. All samples were vacuum annealed to remove as much work hardening as possible.

White and Woods suggest that the electrical resistivity of tantalum at lower temperatures follows more nearly a  $T^{3.8}$  proportionality than a  $T^5$  proportionality. However,



in the section of their report devoted to the error analysis of the electrical resistivity measurements they indicate the difficulties in determining the low-temperature ideal resistivities.

## RESULTS AND DISCUSSION

The program was executed by using 19 of White and Woods experimental values. This involved a temperature range from 10 to 250 K. The resultant values of the parameters were  $A = 39.95$  microhm-centimeters and  $\theta_R = 217.54$  K. The resultant fit of the calculated data to the experimental points is shown in figure 3. It can be seen that the agreement is excellent. The tabular results are shown in appendix C.

The three values of Cox were analyzed by using the code. This involved a temperature range of 77.3 to 373.4 K. The result of this analysis were  $A = 39.51$  microhm-centimeters and  $\theta_R = 210.77$  K. The resulting fit of the data is in figure 4.

Because of the rather limited nature of the Cox data, both the White and Woods data and the Cox data were analyzed together. The resulting fit is shown in figure 5. It can be clearly seen that the Cox data appear higher than the White and Woods data. This indicates either that the residual resistivity of the Cox sample had not been subtracted from the individual values or that the sample had been insufficiently annealed. Thus, the Cox data have been rejected in following the analysis.

As an illustrative example of the utility of the code, the White and Woods data have been analyzed parametrically by using the highest temperature involved as a parameter. The lowest temperature in all these cases was 10 K. The results are shown in figures 6 and 7. The results are tabulated in table III. They show both  $A$  and  $\theta_R$  increasing to their asymptotic values. These are typical results for metallic samples (ref. 4). The characteristic temperature of resistivity  $\theta_R$  is not to be confused with  $\theta_D$ , the Debye characteristic temperature (ref. 13).

It should be indicated at this point that while these results might be obtained by extensive hand calculation, the results shown were obtained in a fraction of a minute by an IBM 7094-II computer.

## SUMMARY OF RESULTS

A computer program was written for evaluation of Bloch-Grueneisen parameters of metals and evaluation of electrical resistivity of tantalum as a function of temperature, and the following results were obtained:

1. The values of the Bloch-Grueneisen parameters for the data of White and Woods were a constant of the metal  $A = 39.95$  microhm-centimeters and a characteristic temperature of resistivity  $\theta_R = 217.54$  K over the temperature range from 10 to 250 K.
2. The results of Cox apparently were not adjusted to ideal resistivity values.
3. When the Bloch-Grueneisen parameters were plotted as a function of the highest temperature used, for tantalum, they reached their asymptotic values at roughly a temperature of  $\theta_R$ .

Lewis Research Center,  
National Aeronautics and Space Administration,  
Cleveland, Ohio, April 19, 1971,  
129-02.

## APPENDIX A

### PROGRAM DESCRIPTION

#### Program Input Data

The card input to the program consists of a temperature  $T_i$ ,  $\rho_{T,i}$ , the source of the data, and the first guess for  $A$  and  $\theta_R$ . The format for these cards is 2F10.0,3X,A6. The user supplies as many cards with  $T_i$ ,  $\rho_{T,i}$ , and the source as needed. The last card contains the first guess for  $A$  and  $\theta_R$  with the field for the source left blank. This card causes the start of the least-squares curve fit. If the user wants the preceding values of  $A$  and  $\theta_R$  as first guesses, the last card should be left entirely blank.

The user may add coding of his own, starting after statement number 7 (card number 37). By punching END on a data card starting in card column 24, the user may execute this coding. This END card causes the program to transfer to statement 7.

#### Program Output

The program output consists of a tabulation of the input data along with  $\rho_c T_i$ , the calculated value of  $\rho_{T,i}$  as defined by the Bloch-Grueneisen relation, and the difference between  $\rho_c T_i$  and  $\rho_{T,i}$ . The values of  $A$ ,  $\theta_R$ , and the sum of the differences squared are also printed. An example of this output is found in appendix C.

## APPENDIX B

### FORTRAN LISTING OF PROGRAM AND OUTPUT

	COMMON /BLOCK/ T(100),RHO(100),RHOC(100),I	A	1
	COMMON /SPACE/ WORK(10)	A	2
	COMMON /ESTIM/ EST, EPS, LIMIT, IER	A	3
	EXTERNAL FAT	A	4
	DIMENSION GRAD(2), X(2), SOURCE(100)	A	5
	EQUIVALENCE (X(1),A), (X(2),THETA)	A	6
	DATA BLANK/1H /	A	7
	DATA END/3HEND/	A	8
	DATA N/2/	A	9
	WRITE (6,8)	A	10
1	I=1	A	11
2	READ (5,12) T(I),RHO(I),SOURCE(I)	A	12
	IF (SOURCE(I)-BLANK) 3,4,3	A	13
3	CONTINUE	A	14
	IF (SOURCE(I).EQ.END) GO TO 7	A	15
	I=I+1	A	16
	GO TO 2	A	17
4	CONTINUE	A	18
	IF (T(I).EQ.0.) GO TO 5	A	19
C	MAKE A FIRST GUESS AT A AND THETA	A	20
	A=T(I)	A	21
	THETA=RHO(I)	A	22
5	CONTINUE	A	23
	I=I-1	A	24
C	CALL THE FLETCHER - POWELL SUBROUTINE	A	25
	CALL FLTPWL (FAT,N,X,VAL,GRAD)	A	26
	IF (IER.NE.0) WRITE (6,9) IER	A	27
	WRITE (6,11)	A	28
	DO 6 J=1,I	A	29
	DIF=RHO(J)-RHOC(J)	A	30
	WRITE (6,13) SOURCE(J),T(J),RHO(J),RHOC(J),DIF	A	31
6	CONTINUE	A	32
	WRITE (6,10)	A	33
	WRITE (6,14) A,THETA,VAL	A	34
	WRITE (6,8)	A	35
	GO TO 1	A	36
7	CONTINUE	A	37
C	PERFORM ANY OTHER CALCULATIONS HERE	A	38
	STOP	A	39
C		A	40
C		A	41
8	FORMAT (1H1)	A	42
9	FORMAT (10X,4HIER=,I2)	A	43
10	FORMAT (1HK,24X,1HA,16X,5HTHETA,8X,23HSUM OF (DIFFERENCES)**2)	A	44
11	FORMAT (1HK,16X,6HSOURCE,17X,11HTEMPERATURE,13X,3HRHO,12X,14HRHO C	A	45
	1ALCULATED,8X,10HDIFFERENCE)	A	46
12	FORMAT (2F10.0,3X,A6)	A	47
13	FORMAT (17X,A6,7X,4F20.6)	A	48
14	FORMAT (10X,3F20.6)	A	49
	END	A	50-

	SUBROUTINE FAT (N,Q,VLL,GRDD)	B	1
C	THIS SUBROUTINE CALCULATES THE LEAST SQUARES FUNCTION F(X)	B	2
C	AND THE GRADIENT OF THE SAME	B	3
C	IN THIS PART X(1)=A , X(2)=THETA	B	4
	COMMON /BLOCK/ T(100),RHO(100),BGR(100),NCASES	B	5
	COMMON /EXPK/ K	B	6
	DIMENSION X(2), GRDD(1), Q(1), GRAD(2)	B	7
	EXTERNAL FUNKY	B	8
	DO 1 I=1,N	B	9
1	X(I)=Q(I)	B	10
	JOKE=0	B	11
	GO TO 2	B	12
	ENTRY BLAST(Z,Y,VLL)	B	13
	X(1)=Z	B	14
	X(2)=Y	B	15
	JOKE=1	B	16
2	CONTINUE	B	17
	VAL=0.	B	18
	DO 3 I=1,2	B	19
3	GRAD(I)=0.	B	20
	AK=K	B	37
	DO 4 I=1,NCASES	B	21
C	CALCULATE THE BLOCH - GRUENEISEN RELATIONSHIP	B	22
	X2DTI=X(2)/T(I)	B	23
	TIDX2=(T(I)/X(2))*K	B	24
	XX=SIMPS1(0.,X2DTI,FUNKY,L)	B	25
	BGR(I)=X(1)*TIDX2*XX	B	26
C	COMPUTE THE DIFFERENCE BETWEEN THE DATA AND THE B.G.R.	B	27
	DIF=RHO(I)-BGR(I)	B	28
	VAL=VAL+DIF**2	B	29
C	TRANSFER AROUND THE UNWANTED GRADIENT CALCULATIONS WHEN JOKE IS 1	B	30
	IF (JOKE.EQ.1) GO TO 4	B	31
	DIF=2.*DIF	B	32
C	CALCULATE THE COMPONENTS OF THE GRADIENT (GRAD(1) AND GRAD(2))	B	33
	GRAD(1)=GRAD(1)-DIF*TIDX2*XX	B	34
	EXP1=EXP(X2DTI)	B	35
	EXPS=(EXP1+1./EXP1-2.)*T(I)	B	36
	GRAD(2)=GRAD(2)+(AK*BGR(I)/X(2)-X(1)/EXPS)*DIF	B	38
4	CONTINUE	B	39
	VLL=VAL	B	40
	IF (JOKE.EQ.1) RETURN	B	41
	DO 5 II=1,2	B	42
5	GRDD(II)=GRAD(II)	B	43
	RETURN	B	44
	END	B	45-

	FUNCTION FUNKY (X)	C	1
C	THIS FUNCTION CALCULATES THE INTEGRAND IN THE B.G.R.	C	2
	COMMON /EXPK/ K	C	3
	IF (X.EQ.0.) GO TO 1	C	4
	EXP1=EXP(X)	C	5
	FUNKY=EXP1+1./EXP1-2.	C	6
	FUNKY=X**K/FUNKY	C	7
	RETURN	C	8
1	FUNKY=0.	C	9
	RETURN	C	10
	END	C	11-

BLOCK DATA	E	1
COMMON /ESTIM/ EST, EPS, LIMIT, IER	E	2
COMMON /EXPK/ K	E	3
C THE ORDER OF THE BLOCH-GRUENEISEN RELATIONSHIP MAY BE CHANGED.		
C TO DO SO, CHANGE THE VALUE OF K IN THE FOLLOWING DATA STATEMENT.		
DATA K/5/	E	4
DATA EST, EPS, LIMIT/1.E-2, 1.E-5, 1000/	E	5
END	E	6-
C SUBROUTINE FLTPWL	F	2
C	F	3
C	F	4
C PURPOSE	F	5
C TO FIND A LOCAL MINIMUM OF A FUNCTION OF SEVERAL VARIABLES	F	6
C BY THE METHOD OF FLETCHER AND POWELL	F	7
C	F	8
C USAGE	F	9
C CALL FLTPWL(FUNCT, N, X, F, G)	F	10
C	F	11
C DESCRIPTION OF PARAMETERS	F	12
C FUNCT - USER-WRITTEN SUBROUTINE CONCERNING THE FUNCTION TO	F	13
C BE MINIMIZED. IT MUST BE OF THE FORM	F	14
C SUBROUTINE FUNCT(N, ARG, VAL, GRAD)	F	15
C AND MUST SERVE THE FOLLOWING PURPOSE	F	16
C FOR EACH N-DIMENSIONAL ARGUMENT VECTOR ARG,	F	17
C FUNCTION VALUE AND GRADIENT VECTOR MUST BE COMPUTED	F	18
C AND, ON RETURN, STORED IN VAL AND GRAD RESPECTIVELY	F	19
C N - NUMBER OF VARIABLES	F	20
C X - VECTOR OF DIMENSION N CONTAINING THE INITIAL	F	21
C ARGUMENT WHERE THE ITERATION STARTS. ON RETURN,	F	22
C X HOLDS THE ARGUMENT CORRESPONDING TO THE	F	23
C COMPUTED MINIMUM FUNCTION VALUE	F	24
C F - SINGLE VARIABLE CONTAINING THE MINIMUM FUNCTION	F	25
C VALUE ON RETURN, I.E. F=F(X).	F	26
C G - VECTOR OF DIMENSION N CONTAINING THE GRADIENT	F	27
C VECTOR CORRESPONDING TO THE MINIMUM ON RETURN,	F	28
C I.E. G=G(X).	F	29
C EST - IS AN ESTIMATE OF THE MINIMUM FUNCTION VALUE.	F	30
C EPS - TESTVALUE REPRESENTING THE EXPECTED ABSOLUTE ERROR.	F	31
C A REASONABLE CHOICE IS 10**(-6), I.E.	F	32
C SOMEWHAT GREATER THAN 10**(-D), WHERE D IS THE	F	33
C NUMBER OF SIGNIFICANT DIGITS IN FLOATING POINT	F	34
C REPRESENTATION.	F	35
C LIMIT - MAXIMUM NUMBER OF ITERATIONS.	F	36
C IER - ERROR PARAMETER	F	37
C IER = 0 MEANS CONVERGENCE WAS OBTAINED	F	38
C IER = 1 MEANS NO CONVERGENCE IN LIMIT ITERATIONS	F	39
C IER = -1 MEANS ERRORS IN GRADIENT CALCULATION	F	40
C IER = 2 MEANS LINEAR SEARCH TECHNIQUE INDICATES	F	41
C IT IS LIKELY THAT THERE EXISTS NO MINIMUM.	F	42
C H - WORKING STORAGE OF DIMENSION N*(N+7)/2.	F	43
C	F	44
C REMARKS	F	45
C 1) THE SUBROUTINE NAME REPLACING THE DUMMY ARGUMENT FUNCT	F	46
C MUST BE DECLARED AS EXTERNAL IN THE CALLING PROGRAM.	F	47

C	II) IER IS SET TO 2 IF , STEPPING IN ONE OF THE COMPUTED	F	48
C	DIRECTIONS. THE FUNCTION WILL NEVER INCREASE WITHIN	F	49
C	A TOLERABLE RANGE OF ARGUMENT.	F	50
C	IER = 2 MAY OCCUR ALSO IF THE INTERVAL WHERE F	F	51
C	INCREASES IS SMALL AND THE INITIAL ARGUMENT WAS	F	52
C	RELATIVELY FAR AWAY FROM THE MINIMUM SUCH THAT THE	F	53
C	MINIMUM WAS OVERLEAPED. THIS IS DUE TO THE SEARCH	F	54
C	TECHNIQUE WHICH DOUBLES THE STEPSIZE UNTIL A POINT	F	55
C	IS FOUND WHERE THE FUNCTION INCREASES.	F	56
C		F	57
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	F	58
C	FUNCT	F	59
C		F	60
C	METHOD	F	61
C	THE METHOD IS DESCRIBED IN THE FOLLOWING ARTICLE	F	62
C	R. FLETCHER AND M.J.D. POWELL, A RAPID DESCENT METHOD FOR	F	63
C	MINIMIZATION,	F	64
C	COMPUTER JOURNAL VOL.6, ISS. 2, 1963, PP.163-168.	F	65
C	THIS SUBROUTINE IS A MODIFICATION OF THE FMFP PROGRAM FROM THE IBM	F	66
C	SCIENTIFIC SUBROUTINE PACKAGE	F	67
C		F	70
	SUBROUTINE FLTPWL (FUNCT,N,X,F,G)	F	71
	COMMON /ESTIM/ EST,EPS,LIMIT,IER	F	72
	COMMON /SPACE/ H(1)	F	73
C		F	74
C	DIMENSIONED DUMMY VARIABLES	F	75
	DIMENSION X(1), G(1)	F	76
C		F	77
C	COMPUTE FUNCTION VALUE AND GRADIENT VECTOR FOR INITIAL ARGUMENT	F	78
	CALL FUNCT (N,X,F,G)	F	79
C		F	80
C	RESET ITERATION COUNTER AND GENERATE IDENTITY MATRIX	F	81
	IER=0	F	82
	KOUNT=0	F	83
	N2=N+N	F	84
	N3=N2+N	F	85
	N31=N3+1	F	86
1	K=N31	F	87
	DO 4 J=1,N	F	88
	H(K)=1.	F	89
	NJ=N-J	F	90
	IF (NJ) 5,5,2	F	91
2	DO 3 L=1,NJ	F	92
	KL=K+L	F	93
3	H(KL)=0.	F	94
4	K=KL+1	F	95
C		F	96
C	START ITERATION LOOP	F	97
5	KOUNT=KOUNT+1	F	98
C		F	99
C	SAVE FUNCTION VALUE, ARGUMENT VECTOR AND GRADIENT VECTOR	F	100
	ULDF=F	F	101
	DO 9 J=1,N	F	102
	K=N+J	F	103
	H(K)=G(J)	F	104
	K=K+N	F	105
	H(K)=X(J)	F	106
C		F	107
C	DETERMINE DIRECTION VECTOR H	F	108
	K=J+N3	F	109
	T=0.	F	110

	DO 8 L=1,N	F 111
	T=T-G(L)*H(K)	F 112
	IF (L-J) 6,7,7	F 113
6	K=K+N-L	F 114
	GO TO 8	F 115
7	K=K+1	F 116
8	CONTINUE	F 117
9	H(J)=T	F 118
C		F 119
C	CHECK WHETHER FUNCTION WILL DECREASE STEPPING ALONG H.	F 120
	DY=0.	F 121
	HNRM=0.	F 122
	GMRM=0.	F 123
C		F 124
C	CALCULATE DIRECTIONAL DERIVATIVE AND TESTVALUES FOR DIRECTION	F 125
C	VECTOR H AND GRADIENT VECTOR G.	F 126
	DO 10 J=1,N	F 127
	HNRM=HNRM+ABS(H(J))	F 128
	GMRM=GMRM+ABS(G(J))	F 129
10	DY=DY+H(J)*G(J)	F 130
C		F 131
C	REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF DIRECTIONAL	F 132
C	DERIVATIVE APPEARS TO BE POSITIVE OR ZERO.	F 133
	IF (DY) 11,54,54	F 134
C		F 135
C	REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF DIRECTION	F 136
C	VECTOR H IS SMALL COMPARED TO GRADIENT VECTOR G.	F 137
11	IF (HNRM/GMRM-EPS) 54,54,12	F 138
C		F 139
C	SEARCH MINIMUM ALONG DIRECTION H	F 140
C		F 141
C	SEARCH ALONG H FOR POSITIVE DIRECTIONAL DERIVATIVE	F 142
12	FY=F	F 143
	ALFA=2.*(EST-F)/DY	F 144
	AMBDA=1.	F 145
C		F 146
C	USE ESTIMATE FOR STEPSIZE ONLY IF IT IS POSITIVE AND LESS THAN	F 147
C	1. OTHERWISE TAKE 1. AS STEPSIZE	F 148
	IF (ALFA) 15,15,13	F 149
13	IF (ALFA-AMBDA) 14,15,15	F 150
14	AMBDA=ALFA	F 151
15	ALFA=0.	F 152
C		F 153
C	SAVE FUNCTION AND DERIVATIVE VALUES FOR OLD ARGUMENT	F 154
16	FX=FY	F 155
	DX=DY	F 156
C		F 157
C	STEP ARGUMENT ALONG H	F 158
	DO 17 I=1,N	F 159
17	X(I)=X(I)+AMBDA*H(I)	F 160
C		F 161
C	COMPUTE FUNCTION VALUE AND GRADIENT FOR NEW ARGUMENT	F 162
	CALL FUNCT (N,X,F,G)	F 163
	FY=F	F 164
C		F 165
C	COMPUTE DIRECTIONAL DERIVATIVE DY FOR NEW ARGUMENT. TERMINATE	F 166
C	SEARCH. IF DY IS POSITIVE. IF DY IS ZERO THE MINIMUM IS FOUND	F 167
	DY=0.	F 168
	DO 18 I=1,N	F 169
18	DY=DY+G(I)*H(I)	F 170
	IF (DY) 19,39,22	F 171
C		F 172



C	TERMINATE SEARCH ALSO IF THE FUNCTION VALUE INDICATES THAT	F 173
C	A MINIMUM HAS BEEN PASSED	F 174
19	IF (FY-FX) 20,22,22	F 175
C		F 176
C	REPEAT SEARCH AND DOUBLE STEPSIZE FOR FURTHER SEARCHES	F 177
20	AMBDA=AMBDA+ALFA	F 178
	ALFA=AMBDA	F 179
C	END OF SEARCH LOOP	F 180
C		F 181
C	TERMINATE IF THE CHANGE IN ARGUMENT GETS VERY LARGE	F 182
	IF (HNRM*AMBDA-1.E10) 16,16,21	F 183
C		F 184
C	LINEAR SEARCH TECHNIQUE INDICATES THAT NO MINIMUM EXISTS	F 185
21	IER=2	F 186
	RETURN	F 187
C		F 188
C	INTERPOLATE CUBICALLY IN THE INTERVAL DEFINED BY THE SEARCH	F 189
C	ABOVE AND COMPUTE THE ARGUMENT X FOR WHICH THE INTERPOLATION	F 190
C	POLYNOMIAL IS MINIMIZED	F 191
22	T=0.	F 192
23	IF (AMBDA) 24,39,24	F 193
24	Z=3.*(FX-FY)/AMBDA+DX+DY	F 194
	ALFA=AMAX1(ABS(Z),ABS(DX),ABS(DY))	F 195
	DALFA=Z/ALFA	F 196
	DALFA=DALFA*DALFA-DX/ALFA*DY/ALFA	F 197
	IF (DALFA) 54,25,25	F 198
25	W=ALFA*SQRT(DALFA)	F 199
	ALFA=DY-DX+W+W	F 200
	IF (ALFA) 26,27,26	F 201
26	ALFA=(DY-Z+W)/ALFA	F 202
	GO TO 28	F 203
27	ALFA=(Z+DY-W)/(Z+DZ+Z+DY)	F 204
28	ALFA=ALFA*AMBDA	F 205
	DO 29 I=1,N	F 206
29	X(I)=X(I)+(T-ALFA)*H(I)	F 207
C		F 208
C	TERMINATE, IF THE VALUE OF THE ACTUAL FUNCTION AT X IS LESS	F 209
C	THAN THE FUNCTION VALUES AT THE INTERVAL ENDS. OTHERWISE REDUCE	F 210
C	THE INTERVAL BY CHOOSING ONE END-POINT EQUAL TO X AND REPEAT	F 211
C	THE INTERPOLATION. WHICH END-POINT IS CHOSEN DEPENDS ON THE	F 212
C	VALUE OF THE FUNCTION AND ITS GRADIENT AT X	F 213
C		F 214
	CALL FNCT (N,X,F,G)	F 215
	IF (F-FX) 30,30,31	F 216
30	IF (F-FY) 39,39,31	F 217
31	DALFA=0.	F 218
	DO 32 I=1,N	F 219
32	DALFA=DALFA+G(I)*H(I)	F 220
	IF (DALFA) 33,36,36	F 221
33	IF (F-FX) 35,34,36	F 222
34	IF (DX-DALFA) 35,39,35	F 223
35	FX=F	F 224
	DX=DALFA	F 225
	T=ALFA	F 226
	AMBDA=ALFA	F 227
	GO TO 23	F 228
36	IF (FY-F) 38,37,38	F 229
37	IF (DY-DALFA) 38,39,38	F 230
38	FY=F	F 231
	DY=DALFA	F 232
	AMBDA=AMBDA-ALFA	F 233
	GO TO 22	F 234

C		F 235
C	TERMINATE, IF FUNCTION HAS NOT DECREASED DURING LAST ITERATION	F 236
39	IF (OLD-F+EPS) 54,40,40	F 237
C		F 238
C	COMPUTE DIFFERENCE VECTORS OF ARGUMENT AND GRADIENT FROM	F 239
C	TWO CONSECUTIVE ITERATIONS	F 240
40	DO 41 J=1,N	F 241
	K=N+J	F 242
	H(K)=G(J)-H(K)	F 243
	K=N+K	F 244
41	H(K)=X(J)-H(K)	F 245
C	TEST LENGTH OF ARGUMENT DIFFERENCE VECTOR AND DIRECTION VECTOR	F 246
C	IF AT LEAST N ITERATIONS HAVE BEEN EXECUTED. TERMINATE, IF	F 247
C	BOTH ARE LESS THAN EPS	F 248
	IER=0	F 249
	IF (KOUNT-N) 45,42,42	F 250
42	T=0.	F 251
	Z=0.	F 252
	DO 43 J=1,N	F 253
	K=N+J	F 254
	w=H(K)	F 255
	K=K+N	F 256
	T=T+ABS(H(K))	F 257
43	Z=Z+w*H(K)	F 258
	IF (HNRM-EPS) 44,44,45	F 259
44	IF (T-EPS) 59,59,45	F 260
C		F 261
C	TERMINATE, IF NUMBER OF ITERATIONS WOULD EXCEED LIMIT	F 262
45	IF (KOUNT-LIMIT) 46,53,53	F 263
C		F 264
C	PREPARE UPDATING OF MATRIX H	F 265
46	ALFA=0.	F 266
	DO 50 J=1,N	F 267
	K=J+N3	F 268
	w=0.	F 269
	DO 49 L=1,N	F 270
	KL=N+L	F 271
	w=w+H(KL)*H(K)	F 272
	IF (L-J) 47,48,48	F 273
47	K=K+N-L	F 274
	GO TO 49	F 275
48	K=K+1	F 276
49	CONTINUE	F 277
	K=N+J	F 278
	ALFA=ALFA+w*H(K)	F 279
50	H(J)=w	F 280
C		F 281
C	REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF RESULTS	F 282
C	ARE NOT SATISFACTORY	F 283
	IF (Z*ALFA) 51,1,51	F 284
C		F 285
C	UPDATE MATRIX H	F 286
51	K=N31	F 287
	DO 52 L=1,N	F 288
	KL=N2+L	F 289
	DO 52 J=L,N	F 290
	NJ=N2+J	F 291
	H(K)=H(K)+H(KL)*H(NJ)/Z-H(L)*H(J)/ALFA	F 292
52	K=K+1	F 293
	GO TO 5	F 294
C	END OF ITERATION LOOP	F 295
C		F 296

C	NO CONVERGENCE AFTER LIMIT ITERATIONS	F 297
53	IER=1	F 298
	RETURN	F 299
C		F 300
C	RESTORE OLD VALUES OF FUNCTION AND ARGUMENTS	F 301
54	DO 55 J=1,N	F 302
	K=N2+J	F 303
55	X(J)=H(K)	F 304
	CALL FUNCT (N,X,F,G)	F 305
C		F 306
C	REPEAT SEARCH IN DIRECTION OF STEEPEST DESCENT IF DERIVATIVE	F 307
C	FAILS TO BE SUFFICIENTLY SMALL	F 308
	IF (GNRM-EPS) 58,58,56	F 309
C		F 310
C	TEST FOR REPEATED FAILURE OF ITERATION	F 311
56	IF (IER) 59,57,57	F 312
57	IER=-1	F 313
	GO TO 1	F 314
58	IER=0	F 315
59	RETURN	F 316
	END	F 317-

## APPENDIX C

### EXAMPLES OF PROGRAM OUTPUT

#### Example 1 - White and Woods Data of 1959

SOURCE	TEMPERATURE	RHO	RHO CALCULATED	DIFFERENCE
WHWD59	10.000000	0.003200	0.001020	0.002180
WHWD59	15.000000	0.017000	0.007719	0.009281
WHWD59	20.000000	0.051000	0.031382	0.019618
WHWD59	25.000000	0.120000	0.086670	0.033330
WHWD59	30.000000	0.230000	0.183421	0.046579
WHWD59	40.000000	0.540000	0.499982	0.040018
WHWD59	50.000000	0.950000	0.936325	0.013675
WHWD59	60.000000	1.430000	1.436732	-0.006732
WHWD59	70.000000	1.960000	1.954969	-0.004969
WHWD59	80.000000	2.500000	2.501859	-0.001859
WHWD59	90.000000	3.030000	3.038230	-0.008230
WHWD59	100.000000	3.550000	3.570093	-0.020093
WHWD59	120.000000	4.600000	4.615721	-0.015721
WHWD59	140.000000	5.600000	5.537964	-0.037964
WHWD59	160.000000	6.650000	6.640883	0.009117
WHWD59	180.000000	7.650000	7.628653	0.021347
WHWD59	200.000000	8.600000	8.604656	-0.004656
WHWD59	220.000000	9.600000	9.571464	0.028536
WHWD59	250.000000	11.000000	11.008536	-0.008536
A	THETA	SUM OF (DIFFERENCES)**2		
39.950176	217.537354	0.009226		

#### Example 2 - Cox Data of 1943

SOURCE	TEMPERATURE	RHO	RHO CALCULATED	DIFFERENCE
MCOX43	77.330000	2.460000	2.464481	-0.004481
MCOX43	273.200001	12.410000	12.389841	0.020159
MCOX43	373.400002	17.180000	17.193873	-0.013873
A	THETA	SUM OF (DIFFERENCES)**2		
39.512384	210.770609	0.000619		

### Example 3 - Cox Data of 1943 and White and Woods Data of 1959

SOURCE	TEMPERATURE	RHO	RHO CALCULATED	DIFFERENCE
WHW059	10.000000	0.003200	0.000929	0.002271
WHW059	15.000000	0.017000	0.007037	0.009963
WHW059	20.000000	0.051000	0.028769	0.022231
WHW059	25.000000	0.120000	0.080298	0.039702
WHW059	30.000000	0.230000	0.171999	0.058001
WHW059	40.000000	0.540000	0.478832	0.051168
WHW059	50.000000	0.950000	0.910253	0.039747
WHW059	60.000000	1.430000	1.411158	0.018842
WHW059	70.000000	1.960000	1.943838	0.016162
WHW059	80.000000	2.500000	2.487599	0.012401
WHW059	90.000000	3.030000	3.032195	-0.002195
WHW059	100.000000	3.550000	3.572969	-0.022969
WHW059	120.000000	4.600000	4.637077	-0.037077
WHW059	140.000000	5.600000	5.677648	-0.077648
WHW059	160.000000	6.650000	6.698330	-0.048330
WHW059	180.000000	7.650000	7.703241	-0.053241
WHW059	200.000000	8.600000	8.695818	-0.095818
WHW059	220.000000	9.600000	9.678715	-0.078715
WHW059	250.000000	11.000000	11.139177	-0.139177
MCOX43	77.330000	2.460000	2.342040	0.117960
MCOX43	273.200001	12.410000	12.259842	0.150158
MCOX43	373.400002	17.180000	17.045341	0.134659
A	THETA	SUM OF (DIFFERENCES)**2		
41.621598	223.468170	0.114080		

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TABLE I. - COX DATA OF 1943

Temperature, K	Total electrical resistivity, $\rho$ , $\mu\text{ohm-cm}$
77.33	2.46
273.2	12.41
373.4	17.18

TABLE II. - WHITE AND WOODS  
DATA OF 1959

Temperature, K	Total electrical resistivity, $\rho$ , $\mu\text{ohm-cm}$
10	0.0032
15	.017
20	.051
25	.12
30	.23
40	.54
50	.95
60	1.43
70	1.96
80	2.50
90	3.03
100	3.55
120	4.60
140	5.60
160	6.65
180	7.65
200	8.60
220	9.6
250	11.0
273	12.1
295	13.1

TABLE III. - BLOCH-GRUENEISEN CONSTANTS AS FUNCTION  
OF MAXIMUM TEMPERATURE

Maximum temperature, K	Constant of metal, $A$ , $\mu\text{ohm-cm}$	Characteristic temperature of resistivity, $\theta_R$ , K
50	27.730	185.664
60	31.233	194.136
70	34.525	202.274
80	36.568	207.447
90	37.530	209.995
100	37.905	211.035
120	38.588	213.063
140	38.726	213.490
160	39.372	215.580
180	39.777	216.932
200	39.813	217.056
220	40.010	217.758
250	39.950	217.537

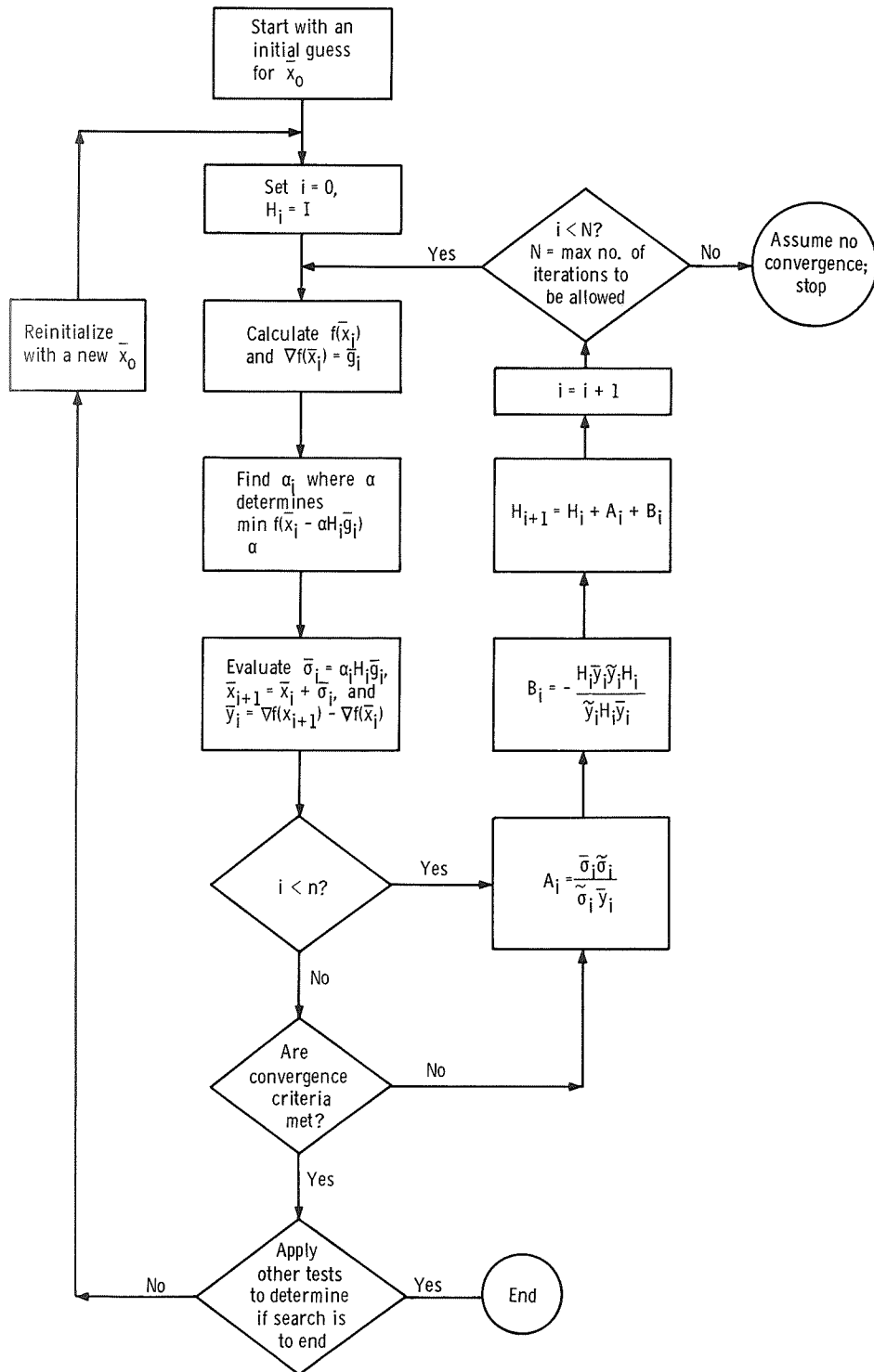


Figure 1. - Fletcher-Powell algorithm.



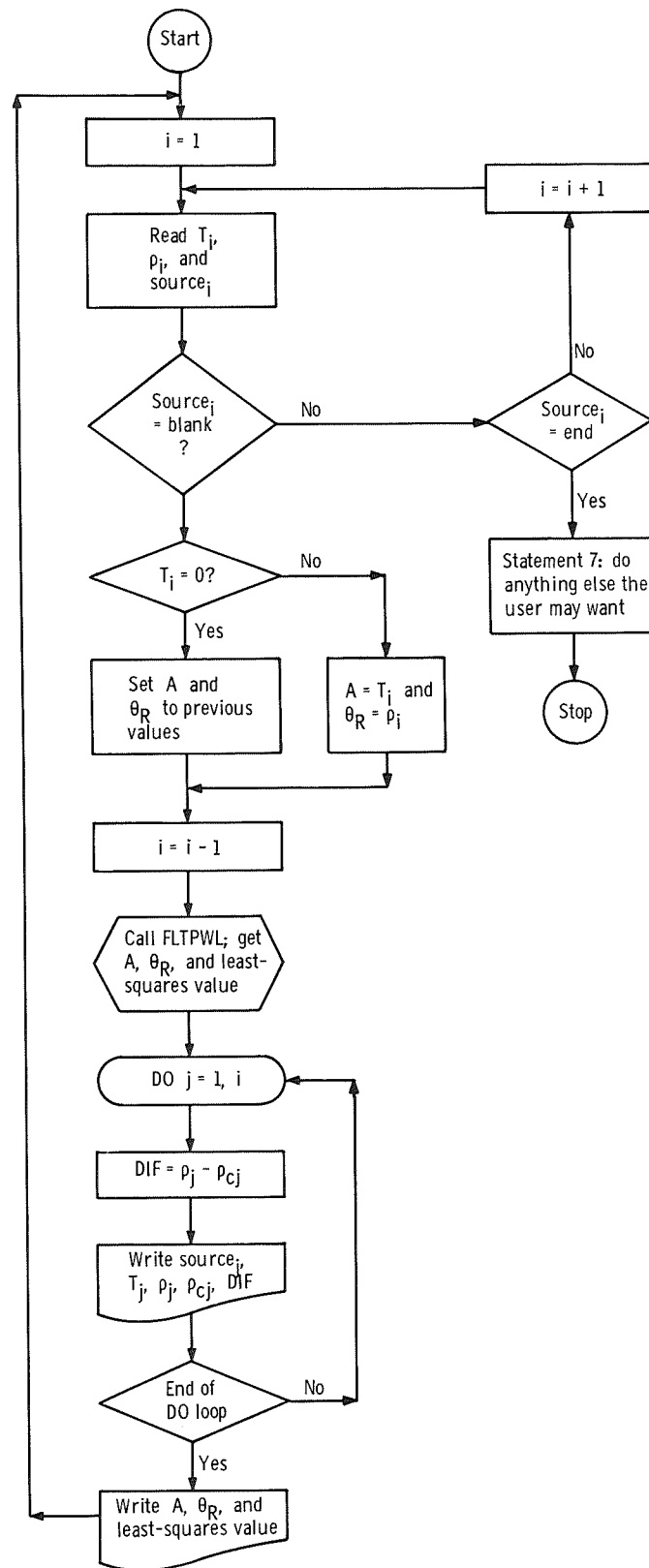


Figure 2. - Main program.

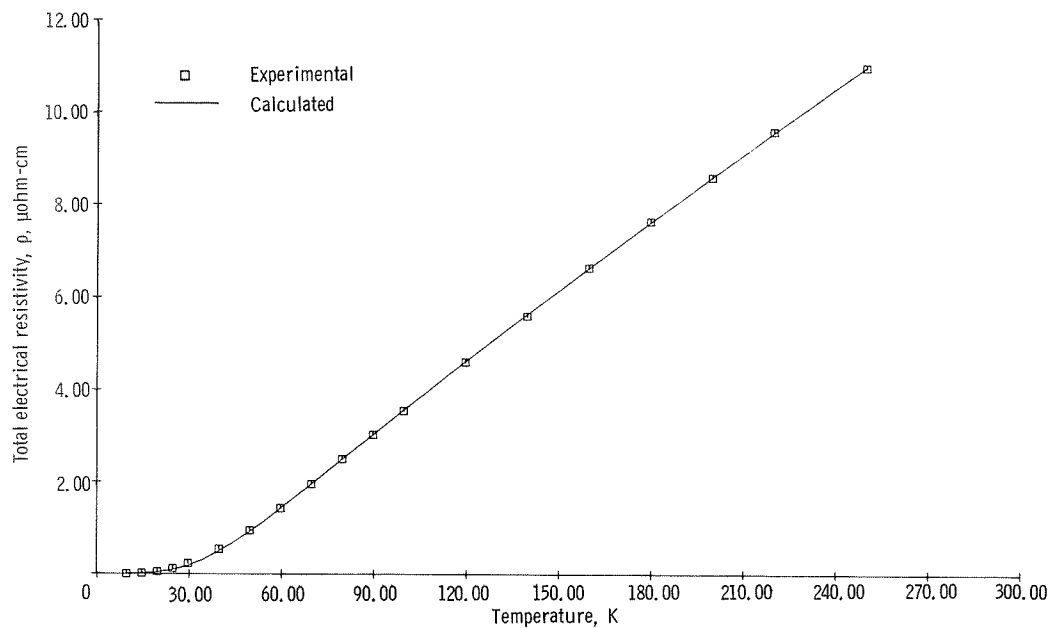


Figure 3. - Fit of White and Woods data.

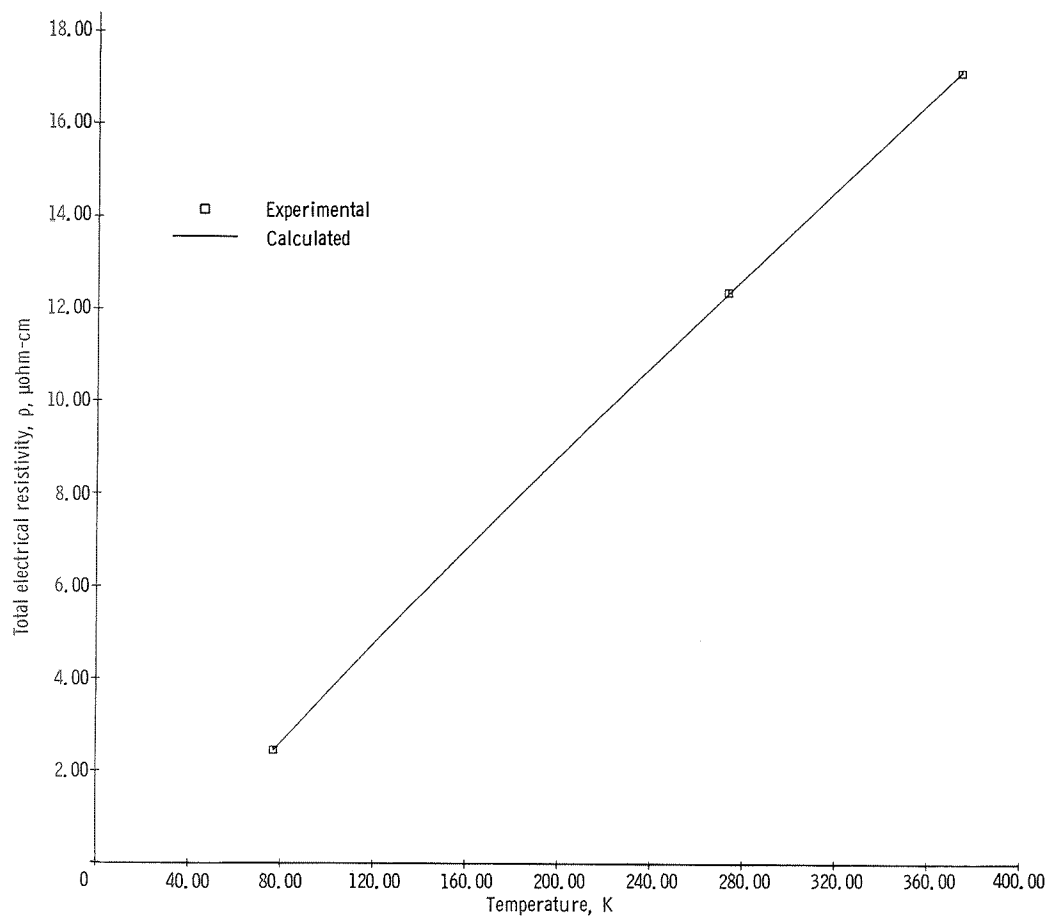


Figure 4. - Fit of Cox data.

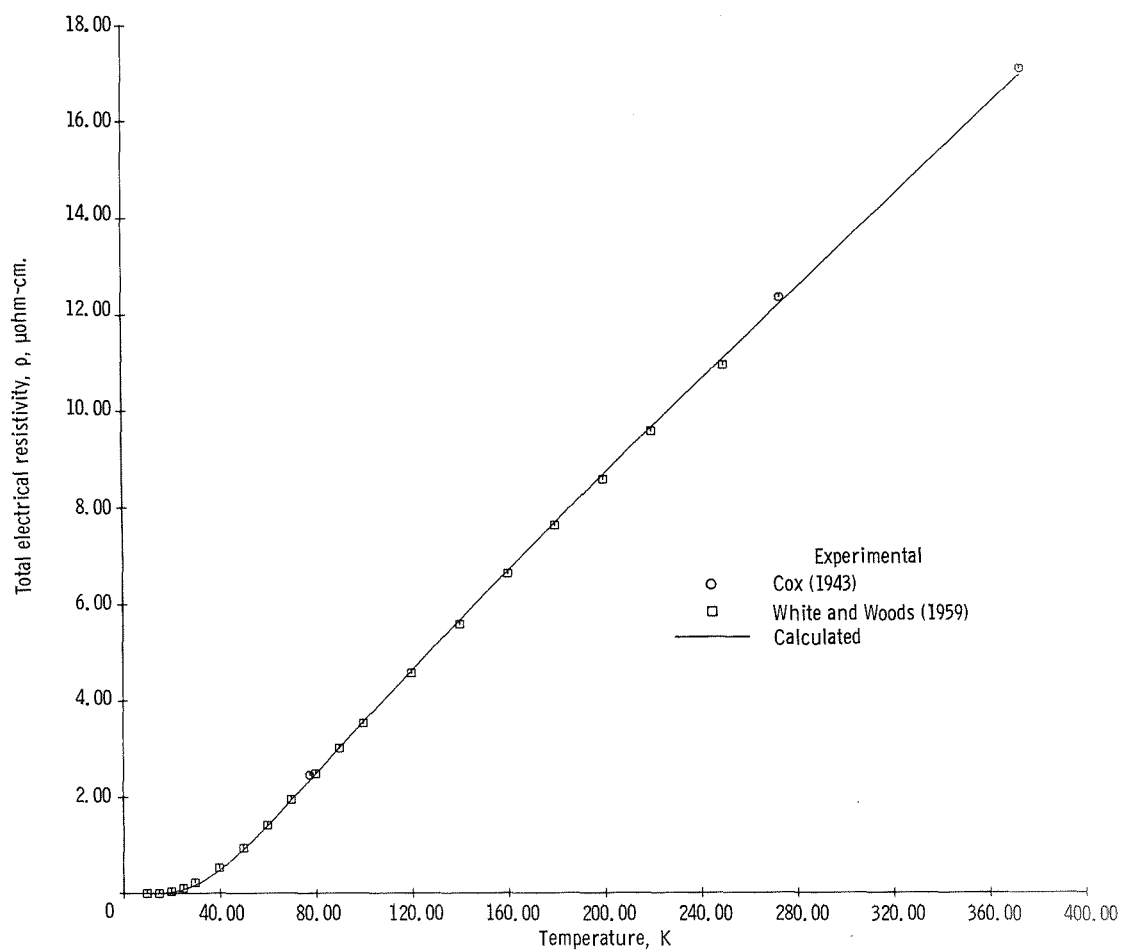


Figure 5. - Fit of Cox data of 1943 with White and Woods data of 1959.

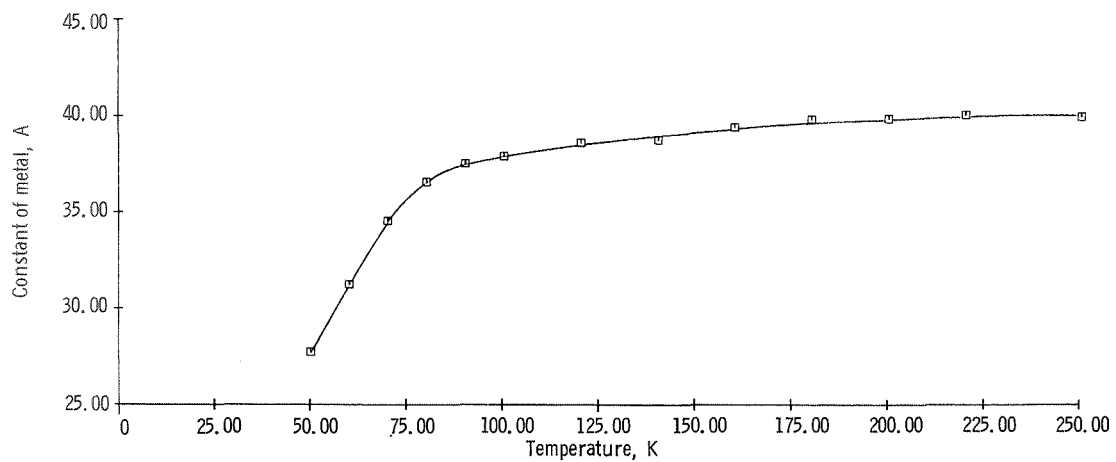


Figure 6. - Constant of metal as function of highest temperature used.

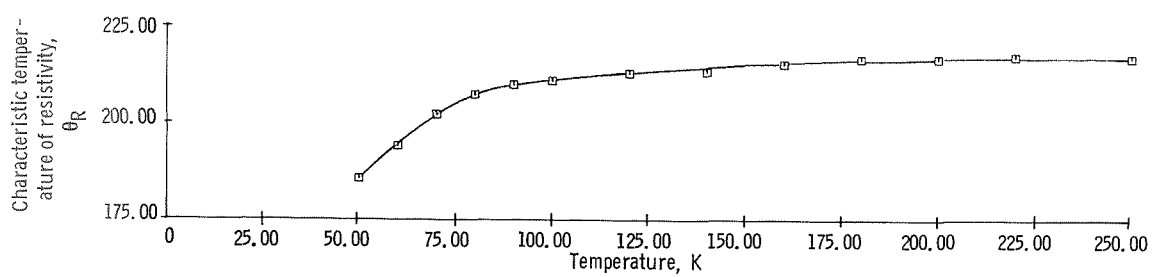


Figure 7. - Characteristic temperature of resistivity as function of maximum temperature used.

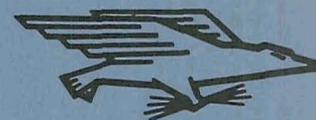
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